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GEOTHERMAL DATA

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GEOTHERMAL GRADIENT DATA AND MAP FOR THE UNITED STATES

The National Geophysical Data Center (NGDC) has produced a new multicolor Geothermal Gradient Map of the United States (exclusive of Alaska and Hawaii). This map, a joint publication of NGDC and Los Alamos National Laboratory (LANL), replaces the 1980 version of the map published by LANL. The new map presents a compilation of over 1,700 wells that have been measured for temperature at depths greater than 50 m. Temperature/depth profiles are linear, or composed of linear segments which reflect changes in the thermal conductivity of the rocks, rather than hydrology. The data are displayed on two sheets (Eastern and Western U.S.) at a scale of 1:2,500,000 in a format which shows the location, depth, and gradient of each well in a single color-coded symbol (see Figure 1). Each well is numbered and keyed to a table showing latitude, longitude, well depth, gradient, heat flow (where available), thermal conductivity (where available), and a reference (see Figure 1). Over 200 references have been consulted and are presented with the data.

In areas where wells are clustered, an average gradient for the area was determined. If the gradients in an area are similar for similar depth intervals, the gradients from several boreholes were averaged. In areas where gradients differ greatly, an average was calculated from a representative sampling of the various anomalous gradients. The location listed in the table is a center point for all the boreholes averaged in a region; the depth represents the deepest well. If a well is significantly deeper than nearby wells, the gradient for the deepest well was chosen.

The quest for geothermal energy during the 1970's and 1980's promoted extensive temperature surveys across the United States. Measuring temperatures in wells has always been the preliminary exploration tool in searching for both hydro-thermal and hot dry rock geothermal systems. In 1976 the American Association of Petroleum Geologists and the U.S. Geological Survey (USGS) published a geothermal gradient map of North America using predominantly bottom-hole temperatures from oil and gas wells. The gradients were calculated using the average annual surface temperature as one point and a corrected temperature at the greatest depth as the second point.

The new map presents gradients from wells that were logged specifically for temperature; that is, the temperature was measured at regular depth intervals in a well that had attained thermal equilibrium, and the slope was calculated for the least-squares line passing through a plot of the data points. This temperature log provided information that enabled an interpretation of the conductive vs. convective component of heat transfer in the underlying rocks.



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CHOOSING, CALCULATING, AND AVERAGING GRADIENTS

The purpose of this map is to present gradients from wells that are in thermal equilibrium and appear to reflect a conductive regime. Only the linearity of the temperature/depth profile is used to determine if the gradient reflects a dominantly conductive regime. Other information concerning the hydrologic nature of the system is not considered. This method presents a consistent approach to evaluating data of highly variable quality, which can also be very inconsistent over small distances due to local changes in hydrology and geology. Where temperature/depth profiles are not available, a quality rating by the original author is considered. It is important to emphasize that gradients shown on this map reflect only the local conditions within a well and cannot be assumed to represent a regional value or to extend below the depth of actual measurement.

The following list specifies criteria used for selecting gradients for the map:

- 1. Wells must be deeper than 50 m.
- Temperature/depth profiles should reflect minimum hydrologic disturbances (i.e., they should approximate a straight line, or consist of straight-line segments that reflect changes in the thermal conductivity of the rocks).
- 3. Gradients must be positive below the temperature inversion due to seasonal effects.
- Only gradients given a high-quality rating by authors are used (generally, a least-squares line with a correlation coefficient of 10%).

Once a gradient met the above criteria, the following methods were used to calculate a representative measurement for the well:

- 1. Gradients were calculated from measurements taken beneath the temperature inversion caused by changes in seasons.
- A least-squares fit was calculated for straight-line segments of a temperature vs. depth plot and a weighted average was determined from these segments.
- 3. In some cases, a straight line was visually drawn to approximate a least-squares fit, and the slope of the line (or straight-line segments) was calculated.
- 4. In Louisiana abundant deep, bottom-hole temperature (BHT) data are available from oil and gas wells. When BHT is plotted against depth for many wells in a region, a least-squares line through the data points approximates the average temperature gradient in that region. The location of such a measurement on the map is the approximate center point of the group of wells considered.



Figure 1. Sample portion of Geothermal Gradient Map. Each well is represented by a symbol which reflects the depth of the deepest temperature measurement, and by a color which represents a gradient interval. The numbers are keyed to a table (see sample at bottom of figure) showing latitude, longitude, well depth, gradient, heat flow, thermal conductivity, and a reference.

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The cost of the map is \$10 folded or \$12 flat per set (Eastern and Western U.S.). Digital data used in making the map are also available in the same format as the list shown on the map. Output may be obtained on magnetic tape for \$200. Please make check or money order payable to COMMERCE/NOAA/NGDC. Orders may also be charged to an American Express card by including card account number, expiration date, and signature. All inquiries should be directed to:

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128 CA 40 50.5 122 36.7 129 CA 40 210 120 54.7 187 34.6 32.6 311 CO 36 107 40.0 75 55.5 35.7 92.2 66 120 CA 40 21.0 121 31.45 226 40.0 310 CO 37 40.0 72. 40.0 72.3 55.54 40.7 55.54 40.7 52.3 55.54 40.0 40.0 40.0 40.0 40.0 40.0 72.0 65 65 65 131 CA 40 14.4 120 70.0 31.6 CO 37 47.0 88 45.0 75.0 66 70.0 71.0	682 MT 45 55. 112 01. 260 19.8 1.8 7.8 22 683 MT 45 43. 112 20. 150 30.1 1.94 6.4 22 684 MT 45 23. 109 54.5 269 19.50 1.52 7.72 2W 685 MT 45 22. 109 49. 253 18.7 1.39 7.8 172 686 MT 45 08. 108 54.1 1742 32.03 1.7 69 688 MT 45 00.5 108 52.2 1525 30.99 1.6 69 727 ND 48 56.1 100 49.6 940 55.0 2.2 4.0 52 730 ND 48 56.3 102 26. 1800 56.0 2.2 4.0 52 730 ND 48 18. 101 40. 1143 39.8 1.4 3.5 18	948 NM 33 53. 106 21. 180 28.84 1.56 155 949 NM 33 45. 107 49. 350 54.40 1.75 3.21 155 950 NM 33 34. 104 30.8 125 16.23 1.44 195 2W 951 NM 33 34. 107 36. 250 61.75 3.36 155 2W 953 NM 33 31. 108 11. 150 61.77 1.98 3.21 155 954 NM 33 19. 107 42. 162 44. 2.92 155 2W 956 NM 33 17.1 107 16.3 160 37.8 1.8 155 170 2W 956 NM 33 11.6 107 14.3 152 34.6 2.0 170 3W 3W 957 NM 33 04.5 107 7.52 51.3 2.5 170 <	1087 NV 37 03. 116 02. 701 42.03 07 172 1088 NV 36 48. 116 24. 290 35.4 1.6 4.4 172 1089 NV 36 46. 116 07. 808 41.77 1.81 4.42 172 1090 NV 36 46. 115 52. 350 39.9 2.2 6.5 172 1091 NV 36 38. 116 18. 244 31.1 2.0 6.3 172 1092 NV 36 36. 115 47. 457 15.7 2.17 14.2 172 1093 NV 35 28. 115 08. 315 25. 2.33 67 168 2W OKLAHOMA 1131 OK 36 59.9 97 18.9 430 35.80 197 216 1133 OK 36 59.6 97 19.8 719 32.66	T261 OR 43 51.4 120 15.3 58 52.9 1.85 3.5 103 105 T262 OR 43 47.94 122 25.06 140 30.4 2.86 37 2W T263 OR 43 47.94 122 18.83 135 60.5 2.70 1.65 26 37 T264 OR 43 47.6 122 319 T34 44.62 26 37 2W T265 OR 43 45.7 118 23.1 100 68.4 2.7 4.0 28 30 T266 OR 43 45.7 118 23.1 100 68.4 2.7 4.0 28 30 T268 OR 43 43.15 122 19.97 150 60.0 2.42 3.99 37 104 1270 OR 43 40.1 117 23. 75 53.5 1.5 2.8 30 1272 OR 43 40.1 117	No. St. Lat. Long. Depth Grad. H.F. T.C. Ref. 1410 UT 41 01.72 113 46.67 155 42.2 2.10 46 1411 UT 40 47. 112 04.3 63 58.72 1.8 3.0 55 1412 UT 40 31.5 112 09. 1156 19.54 1.89 55 67 168<2W 1413 UT 40 26.5 109 38.5 265 13.2 65 65 1414 UT 40 10. 109 18. 2.00 131 143 168 3W 1415 UT 39 55.67 112 03.50 357 70.40 131 143 168 3W 1417 UT 39 52.2 112 0.46 59 446 124 46.85 99 44.80 67 167 168	No. St. Lat. Long. Depth Grad. H.F. T.C. Ref. 1590 WA 46 42.9 121 34.7 115 46.5 117 1590 WA 46 41.8 120 40.7 343 25.1 117 1591 WA 46 41.8 120 40.7 343 25.1 118BHT 1592 WA 46 60.44 121 01.71 153 93.0 184 1593 WA 46 30.07 121 18.43 153 54.24 184 2W 1594 WA 46 35.3 121 23.5 150 50.7 19 117<2W 1595 WA 46 35.4 122 51.1 152 41.8 19 19 197 19 117 2W 1595 WA 46 35.4 122 51.1 122 41.8 19 19 197 19 172 172 1595 WA 46	AGLE PASS
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PN0 CA JY HZ LZ HZ HZ <t< td=""><td>853 NM 36 50 107 55 710 31.80 1.47 155 860 NM 36 49 104 41. 225 38.31 2.13 5.56 80 861 NM 36 47. 107 50. 520 29.01 172 5.94 155 863 NM 36 47. 104 42. 125 61.91 242 67.70 80 864 NM 36 45. 106 48 160 38 1.44 155 866 NM 36 45. 107 43. 450 28.94 1.33 4.59 155 866 NM 36 42. 107 43. 450 28.94 1.33 4.59 155 870 NM 36 30. 107 40 650 27.31 1.26 46.30 155 168 3W 871 NM 36 36. 107 21. 1208 52.3 155 38.72</td><td>1008 NV 41 045 119 011 90 7022 227 320 14 1000 NV 40 55. 116 01. 152 22.2 17 6.68 172 1011 NV 40 55. 119 05.1 17 32.8 155 150 173 1013 NV 40 55.0 119 13.3 102 63.1 15 173 4W 1015 NV 40 45.9 119 13.3 102 63.1 15 173 4W 1016 NV 40 37.1 170 39.3 100 782.2 2.8 174 177 85 10W 1010 NV 40 33.1 177 46.7 166 3.2 73 3.8 85 172 4W 1023 NV 40 33.1 177 66 1410 3.124 350</td><td>1182 OR 45 23.6 721 48.4 1214 60. 2.4 4.5 2.3 1184 OR 45 21.9 118 32.6 280 12.7 104 1186 OR 45 21.5 118 07.5 150 35.3 .06 1186 OR 45 19.70 117 54.18 85 23.6 .24 .43 .24 1180 OR 45 19.77 12.4 42.5 584 74.48 .25 .141 38 1190 OR 45 17.8 121 47.8 400 51.2 2.1 4.04 23 1191 OR 45 17.7 12.1 43.5 20 49.58 .21 .141 380 38 1192 OR 45 13.45 117 51.72 .20 13.0 36.0 1.41 .300 38 1199 OR 45 03.3 122 36.9 170 28.9 .06 .06 .104</td><td>SOUTH DACUT 1356 50 44 12 103 45 2048 2120 0.5 512 172 1357 50 44 103 45 2048 2120 0.5 512 172 1359 50 44 06 103 43 230 520 7.77 0.5 6.70 172 1360 50 43 06 12 100 27 1277 1495 997 26 1371 1X 36 12 100 27 1277 1495 997 26 1373 1X 34 02 98 55 588 22.84 197 26 1373 1X 34 02 98 55 589 21.84 197 26 1373 1X 33 38 100 15 732 16.79 96 197 216 1374 1X 33 04 98 1321 33.41 197 26 1376 1X</td><td>1456 UT 36 0.26 113 24.05 93 40 153 3.82 47 1457 UT 37 59.06 113 57.03 60 49 1.87 3.82 47 1458 UT 37 59.06 113 57.37.03 60 49 1.87 3.82 47 1450 UT 37 59.06 113 57.37.03 60 49 1.87 3.82 47 1460 UT 37 53.00 113 26.20 100 46 160 3.35 47 1461 UT 37 44.33 114 02.32 100 82 3.42 4.30 47 1466 UT 37 43.3 111 09 60 21.6 103 4.04 47 1466 UT 37 43.88 113 33.06 27.78 2.12 172 6W 1469 UT 37 36.88 113 0.10 15.1 158 1.52 160</td><td>1637WA4543.812226.210326.7991638WA4540.012222.612723.0991640WA4538.7812158.0818072.81842W1640WA4538.7812207.712952.7991643WA4535.9212223.8815231.5191.171642WA4536.610226.418828.7191643WA4536.610952.2006.156.92W1659WY4456.610952.2006.12.18.46.91661WY4420.010405.220026.12.18.46.91662WY4420.010405.220026.12.18.46.91664WY4410.01067.030.901.34.01896197.2162W1664WY4356.1810838.6630.536.391.86.97186.9772.61666WY4348.310821.091429.1996197.21621.61667WY4348.310821.091429.1996197.2169W1673WY4348.310821.091429.1996<td< td=""><td>Open colspan="2">Open colspan="2"Open colspan="2">Open colspan="2">Open colspan="2"Open colspan="2">Open colspan="2"Open colspan="2"Op</td></td<></td></t<>	853 NM 36 50 107 55 710 31.80 1.47 155 860 NM 36 49 104 41. 225 38.31 2.13 5.56 80 861 NM 36 47. 107 50. 520 29.01 172 5.94 155 863 NM 36 47. 104 42. 125 61.91 242 67.70 80 864 NM 36 45. 106 48 160 38 1.44 155 866 NM 36 45. 107 43. 450 28.94 1.33 4.59 155 866 NM 36 42. 107 43. 450 28.94 1.33 4.59 155 870 NM 36 30. 107 40 650 27.31 1.26 46.30 155 168 3W 871 NM 36 36. 107 21. 1208 52.3 155 38.72	1008 NV 41 045 119 011 90 7022 227 320 14 1000 NV 40 55. 116 01. 152 22.2 17 6.68 172 1011 NV 40 55. 119 05.1 17 32.8 155 150 173 1013 NV 40 55.0 119 13.3 102 63.1 15 173 4W 1015 NV 40 45.9 119 13.3 102 63.1 15 173 4W 1016 NV 40 37.1 170 39.3 100 782.2 2.8 174 177 85 10W 1010 NV 40 33.1 177 46.7 166 3.2 73 3.8 85 172 4W 1023 NV 40 33.1 177 66 1410 3.124 350	1182 OR 45 23.6 721 48.4 1214 60. 2.4 4.5 2.3 1184 OR 45 21.9 118 32.6 280 12.7 104 1186 OR 45 21.5 118 07.5 150 35.3 .06 1186 OR 45 19.70 117 54.18 85 23.6 .24 .43 .24 1180 OR 45 19.77 12.4 42.5 584 74.48 .25 .141 38 1190 OR 45 17.8 121 47.8 400 51.2 2.1 4.04 23 1191 OR 45 17.7 12.1 43.5 20 49.58 .21 .141 380 38 1192 OR 45 13.45 117 51.72 .20 13.0 36.0 1.41 .300 38 1199 OR 45 03.3 122 36.9 170 28.9 .06 .06 .104	SOUTH DACUT 1356 50 44 12 103 45 2048 2120 0.5 512 172 1357 50 44 103 45 2048 2120 0.5 512 172 1359 50 44 06 103 43 230 520 7.77 0.5 6.70 172 1360 50 43 06 12 100 27 1277 1495 997 26 1371 1X 36 12 100 27 1277 1495 997 26 1373 1X 34 02 98 55 588 22.84 197 26 1373 1X 34 02 98 55 589 21.84 197 26 1373 1X 33 38 100 15 732 16.79 96 197 216 1374 1X 33 04 98 1321 33.41 197 26 1376 1X	1456 UT 36 0.26 113 24.05 93 40 153 3.82 47 1457 UT 37 59.06 113 57.03 60 49 1.87 3.82 47 1458 UT 37 59.06 113 57.37.03 60 49 1.87 3.82 47 1450 UT 37 59.06 113 57.37.03 60 49 1.87 3.82 47 1460 UT 37 53.00 113 26.20 100 46 160 3.35 47 1461 UT 37 44.33 114 02.32 100 82 3.42 4.30 47 1466 UT 37 43.3 111 09 60 21.6 103 4.04 47 1466 UT 37 43.88 113 33.06 27.78 2.12 172 6W 1469 UT 37 36.88 113 0.10 15.1 158 1.52 160	1637WA4543.812226.210326.7991638WA4540.012222.612723.0991640WA4538.7812158.0818072.81842W1640WA4538.7812207.712952.7991643WA4535.9212223.8815231.5191.171642WA4536.610226.418828.7191643WA4536.610952.2006.156.92W1659WY4456.610952.2006.12.18.46.91661WY4420.010405.220026.12.18.46.91662WY4420.010405.220026.12.18.46.91664WY4410.01067.030.901.34.01896197.2162W1664WY4356.1810838.6630.536.391.86.97186.9772.61666WY4348.310821.091429.1996197.21621.61667WY4348.310821.091429.1996197.2169W1673WY4348.310821.091429.1996 <td< td=""><td>Open colspan="2">Open colspan="2"Open colspan="2">Open colspan="2">Open colspan="2"Open colspan="2">Open colspan="2"Open colspan="2"Op</td></td<>	Open colspan="2">Open colspan="2"Open colspan="2">Open colspan="2">Open colspan="2"Open colspan="2">Open colspan="2"Open colspan="2"Op